

# DOA Estimation Exploiting Distributed Array with Arbitrary Subarray Orientations

Yimin D. Zhang<sup>1</sup>, Md Waqeeb T. S. Chowdhury<sup>1</sup>, Yanwu Ding<sup>2</sup>, Dan Shen<sup>3</sup>, Khanh Pham<sup>4</sup>, Erik Blasch<sup>5</sup>, and Genshe Chen<sup>3</sup>

<sup>1</sup> Department of Electrical and Computer Engineering, Temple University, Philadelphia, PA 19122

<sup>2</sup> Department of Electrical and Computer Engineering, Wichita State University, Wichita, KS 67260

<sup>3</sup> Intelligent Fusion Technology, Inc., Germantown, MD 20876

<sup>4</sup> Air Force Research Laboratory, Kirtland Air Force Base, NM 87117

<sup>5</sup> Air Force Research Laboratory, Wright-Patterson Air Force Base, OH 45433

**Abstract** – This paper considers a two-dimensional direction-of-arrival (DOA) estimation problem from a collaborative, distributed antenna array where each subarray is a distributed sensing node that is arbitrarily oriented. While the relative locations of the subarrays are not precisely known, it is assumed that the configuration of each subarray is locally calibrated whereas the cross-covariance matrix between a pair of distributed nodes includes an unknown phase difference. Without explicitly estimating such unknown phase difference, subspace-based DOA estimation methods fail to coherently utilize the subarrays to locate the DOAs of the impinging signals. We propose a group sparsity-based approach to achieve accurate DOA estimation that is resilient to unknown phase disparities between subarrays. Simulation results clearly illustrate the effectiveness of the group sparsity-based approach using group LASSO, and the superiority over subspace-based methods, such as the MUSIC algorithm, is demonstrated.

**Keywords:** Direction-of-arrival estimation, distributed array, sparse array, group sparsity, unmanned aerial vehicle, cube satellite network.

## I. INTRODUCTION

Distributed sensing and source/target localization using distributed arrays have attracted significant interests in recent years [1 – 8]. A collaborative sensing system comprising distributed sensing nodes enables small platforms’ coordination, such as sensor networks, unmanned aerial vehicle (UAV) swarms, and cube satellite (CubeSat) systems [9 – 13]. In particular, a distributed array exploiting multiple closely spaced subarrays provides an effective alternative to large-scale arrays when they cannot be feasibly built on a single platform.

To jointly perform directions-of-arrival (DOA) estimation

based on a distributed array, non-coherent processing of partly-calibrated subarrays is studied in [1, 5]. In [6], collinear subarrays are considered, and covariance matrix completion is used to achieve a full aperture of the distributed array. Parallel sparse arrays are considered in [14] to achieve two-dimensional (2-D) DOA estimation. Mixed-precision data using full-precision self-subarray covariance matrices and one-bit data-based cross-subarray covariance matrices are developed in [7, 8] to achieve full-aperture exploitation and enhanced DOA estimation performance in a communication traffic-limited distributed array system. Direction finding using a partly-calibrated arrays in the presence of position errors is considered in [15].

Most work reported in the literature considers subarrays that are placed in either a collinear or a parallel fashion. Although such assumptions make the analyses simpler, in many practical applications, the subarrays may be placed in arbitrary orientations. In such scenarios, the signal models deviate from those developed for collinear and parallel subarrays. On the other hand, subarrays with different orientations form a 2-D distributed array aperture, thereby enabling 2-D DOA estimation of the scene.

In this paper, we consider a distributed array in which multiple linear subarrays are placed in a plane with arbitrary orientations. The signal model is developed with the consideration of the unknown phase differences between the signals received by these subarrays. The presence of such unknown phase differences impedes the direction application of subspace-based DOA estimation methods, such as Multiple Signal Classification (MUSIC), for coherent processing across the entire array without explicitly estimating these phase differences [16]. In other words, the signals received at the subarrays cannot be coherently combined based on traditional subspace-based DOA estimation methods.

It is interesting to note that such a DOA estimation problem with unknown phase differences between subarrays is analogous to that encountered in the DOA estimation based on multi-frequency and wideband arrays, where the phase differences between the observed signals corresponding to different frequencies is unknown [17–20]. For such problems, group

---

This material is based upon work supported by the Air Force Research Laboratory (AFRL) under Contract No. FA9453-22-C-A127. Any opinions, findings and conclusions or recommendations expressed in this material are those of the authors and do not necessarily reflect the views of the AFRL.

sparsity-based methods, which utilize the shared sparse patterns of the nonzero entries without phase alignment requirement, are known to provide near-coherent signal processing capabilities [21]. In this paper, we use the group Least Absolute Shrinkage and Selection Operator (LASSO) [22, 23] approach to produce robust DOA estimation estimates. Simulation results are provided to verify that, unlike MUSIC which is sensitive to the unknown phase differences between the subarrays, the group LASSO-based approach enables robust DOA estimation without relying on the knowledge of the phase differences.

*Notations:* We use lower-case (upper-case) bold characters to describe vectors (matrices). In particular,  $\mathbf{I}_N$  denotes the  $N \times N$  identity matrix and  $\mathbf{0}$  stands for a vector or matrix with all elements to be zero.  $(\cdot)^*$  represents complex conjugate,  $(\cdot)^T$  and  $(\cdot)^H$  respectively denote the transpose and conjugate transpose of a matrix or a vector.  $\text{diag}(\cdot)$  and  $\text{bdiag}(\cdot)$  respectively form diagonal and block diagonal matrices, and  $\text{vec}(\cdot)$  forms a vector from a matrix.  $\|\cdot\|_2$  and  $\|\cdot\|_{1,2}$  represent the  $l_2$  norm and mixed  $l_{1,2}$  norm of a vector, respectively.  $\mathbb{E}(\cdot)$  performs statistical expectation and  $\otimes$  performs Kronecker product. For a matrix  $\mathbf{A}$ , the element in the  $p$ th row and  $q$ th column is denoted as  $\mathbf{A}(p, q)$ .

## II. SIGNAL MODEL

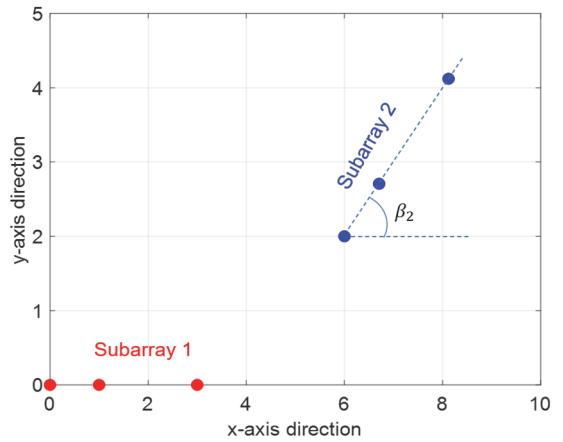
Consider  $K$  arbitrarily oriented linear subarrays, and an example of a distributed array comprising two sparse subarrays is shown in Fig. 1 on a half-wavelength grid. Each subarray can be mounted on a small platform, such as a UAV or a CubeSat. The arrays are located at the same altitude and all antennas are placed in the same  $x$ - $y$  plane. Each subarray is a linear array consisting of  $M_k \geq 2$  sensors which may either be uniformly or sparsely placed [24–27]. The total number of antennas in the distributed array is  $M = \sum_{k=1}^K M_k$ . The configuration of each subarray is calibrated and known, whereas the relative positions of the subarrays are not precisely known.

The nodes are closely located such that the paths from the signals to these nodes are considered parallel, i.e., the subarrays observe the same DOAs of the scene. The position of the  $m$ th antenna in the  $k$ th subarray is denoted as  $(x_{km}, y_{km})$ . We take the first antenna of the first node as the global reference of the array, i.e.,  $(x_{11}, y_{11}) = (0, 0)$ . The orientation of the  $k$ th nodes is denoted as  $\beta_k$  with respect to the  $x$ -axis and is assumed to be known for all  $k$ . Without loss of generality, we assume  $\beta_1 = 0$ .

When  $L$  uncorrelated and far-field signals impinge on the arrays from directions  $(\theta_l, \phi_l)$ ,  $l = 1, \dots, L$ , where  $\theta_l$  and  $\phi_l$  are respectively the elevation and azimuth angles of the  $l$ th signal, the baseband signal vector received at the subarray of the  $k$ th node is expressed as

$$\mathbf{x}^{(k)}(t) = \sum_{l=1}^L s_l(t) e^{-j2\pi\kappa d_l^{(k)}} \mathbf{a}^{(k)}(\theta_l, \phi_l) + \mathbf{n}^{(k)}(t), \quad (1)$$

where  $s_l(t)$  is the waveform of the  $l$ th signal,  $\kappa = f_c/c$  is the wavenumber with  $f_c$  denoting the carrier frequency and  $c$  the propagation velocity of electromagnetic waves in free space,



**Figure 1.** Geometry of a distributed array comprising two 3-element subarrays plotted on a half-wavelength grid.

$d_l^{(k)}$  is the unknown distance between the  $l$ th signal and the reference antenna of the  $k$ th node,  $\mathbf{a}^{(k)}(\theta_l, \phi_l)$  is the steering vector of the subarray at the  $k$ th node towards the  $l$ th signal, and  $\mathbf{n}^{(k)}(t) \sim \mathcal{CN}(\mathbf{0}, \sigma_n^2 \mathbf{I}_{M_k})$  is an additive complex Gaussian noise vector. The steering vector is expressed as

$$\mathbf{a}^{(k)}(\theta_l, \phi_l) = \left[ 1, e^{-j2\pi\kappa p_2^{(k)} u_l^{(k)}}, \dots, e^{-j2\pi\kappa p_{M_k}^{(k)} u_l^{(k)}} \right]^T, \quad (2)$$

where  $p_m^{(k)} = \|x_{km} - x_{k1}, y_{km} - y_{k1}\|_2$  is the distance between the  $m$ th sensor of the  $k$ th node to its local reference at  $(x_{k1}, y_{k1})$ , and  $u_l^{(k)} = \cos(\theta_l) \sin(\phi_l - \beta_k)$ .

Equation (1) can be written as

$$\mathbf{x}^{(k)}(t) = \mathbf{A}^{(k)}(\boldsymbol{\theta}, \boldsymbol{\phi}) \mathbf{V}^{(k)} \mathbf{s}(t) + \mathbf{n}^{(k)}(t), \quad (3)$$

where

$$\mathbf{A}^{(k)}(\boldsymbol{\theta}, \boldsymbol{\phi}) = [\mathbf{a}^{(k)}(\theta_1, \phi_1), \dots, \mathbf{a}^{(k)}(\theta_L, \phi_L)] \quad (4)$$

is the subarray manifold matrix with  $(\boldsymbol{\theta}, \boldsymbol{\phi}) = \{(\theta_1, \phi_1), \dots, (\theta_L, \phi_L)\}$ ,

$$\mathbf{V}^{(k)} = \text{diag} \left[ e^{-j2\pi\kappa d_1^{(k)}}, \dots, e^{-j2\pi\kappa d_L^{(k)}} \right], \quad (5)$$

and  $\mathbf{s}(t) = [s_1(t), \dots, s_L(t)]^T$ .

Cascading the data vectors across all subarrays yields the total received data vector across the entire distributed array as

$$\begin{aligned} \mathbf{x}(t) &= \left[ (\mathbf{x}^{(1)}(t))^T, \dots, (\mathbf{x}^{(K)}(t))^T \right]^T \\ &= \mathbf{A}(\boldsymbol{\theta}, \boldsymbol{\phi}) \mathbf{V} \mathbf{s}(t) + \mathbf{n}(t), \end{aligned} \quad (6)$$

where the effective array manifold, the phase-difference term, and the noise across the entire distributed array are respectively given as

$$\mathbf{A}(\boldsymbol{\theta}, \boldsymbol{\phi}) = \left[ (\mathbf{A}^{(1)}(\boldsymbol{\theta}, \boldsymbol{\phi}))^T, \dots, (\mathbf{A}^{(K)}(\boldsymbol{\theta}, \boldsymbol{\phi}))^T \right]^T, \quad (7)$$

$$\mathbf{V} = \text{bdiag}[\mathbf{V}^{(1)}, \dots, \mathbf{V}^{(K)}], \quad (8)$$

and

$$\mathbf{n}(t) = \left[ \left( \mathbf{n}^{(1)}(t) \right)^T, \dots, \left( \mathbf{n}^{(K)}(t) \right)^T \right]^T. \quad (9)$$

### III. ARRAY COVARIANCE MATRIX

The covariance matrix of the array data vector,  $\mathbf{x}(t)$ , given in (6), is expressed as

$$\mathbf{R} = \mathbb{E}[\mathbf{x}(t)\mathbf{x}^H(t)] = \begin{bmatrix} \mathbf{R}_{11} & \mathbf{R}_{12} & \cdots & \mathbf{R}_{1K} \\ \mathbf{R}_{21} & \mathbf{R}_{22} & \cdots & \mathbf{R}_{2K} \\ \vdots & \vdots & \ddots & \vdots \\ \mathbf{R}_{K1} & \mathbf{R}_{K2} & \cdots & \mathbf{R}_{KK} \end{bmatrix} \quad (10)$$

where

$$\mathbf{R}_{uv} = \mathbb{E}[\mathbf{x}^{(u)}(t)[\mathbf{x}^{(v)}(t)]^H], \quad u, v \in 1, \dots, K. \quad (11)$$

In (11), the cases of  $u = v$  correspond to the self-subarray covariance matrices of the linear subarrays which are well known. On the other hand, when  $u \neq v$ , the cross-covariance matrix between two subarrays is obtained as,

$$\begin{aligned} \mathbf{R}_{uv} &= \mathbb{E}[\mathbf{x}^{(u)}(t)[\mathbf{x}^{(v)}(t)]^H] \\ &= \mathbf{A}^{(u)}(\boldsymbol{\theta}, \boldsymbol{\phi}) \mathbf{V}^{(u)} \mathbf{R}_{ss} [\mathbf{V}^{(v)}]^H [\mathbf{A}^{(v)}(\boldsymbol{\theta}, \boldsymbol{\phi})]^H \\ &= \mathbf{A}^{(u)}(\boldsymbol{\theta}, \boldsymbol{\phi}) \mathbf{R}_{ss}^{(uv)} [\mathbf{A}^{(v)}(\boldsymbol{\theta}, \boldsymbol{\phi})]^H, \end{aligned} \quad (12)$$

where  $\mathbf{R}_{ss} = \mathbb{E}[\mathbf{s}(t)\mathbf{s}^H(t)] = \text{diag}[\rho_1, \dots, \rho_L]$  is the source covariance matrix with  $\rho_l = \mathbb{E}[|s_l(t)|^2]$  being the source power of the  $l$ th signal. In addition,

$$\mathbf{R}_{ss}^{(uv)} = \mathbf{V}^{(u)} \mathbf{R}_{ss} [\mathbf{V}^{(v)}]^H = \text{diag}[\rho_1^{(uv)}, \dots, \rho_L^{(uv)}] \quad (13)$$

is the source cross-correlation matrix between the two subarrays, where  $\rho_l^{(uv)} = \rho_l e^{-j2\pi k[d_l^{(u)} - d_l^{(v)}]}$ ,  $l = 1, \dots, L$ . Note that the phase difference between the two subarrays  $\rho_l^{(uv)}$  is unknown and, in general, takes a complex value. Also notice that  $\mathbf{R}_{21} = \mathbf{R}_{12}^H$ .

### IV. GROUP SPARSITY-BASED DOA ESTIMATION

When applying the MUSIC method to coherently exploit the measurements available to the  $K$  subarrays, we need to know their phase differences in order to form the steering vector corresponding to a direction to be sensed.

As mentioned earlier, the underlying DOA estimation problem is analogous to that encountered in multi-frequency sparse arrays, where the phase differences between the signals corresponding to different frequencies is unknown. However, unlike [18–20] where the virtual arrays obtained from multiple frequencies are collocated, the subarrays in the underlying problems are separated and with different orientations.

To understand the difference coarrays obtained from the two subarrays  $u$  and  $v$ , we vectorize  $\mathbf{R}_{uv}$  in (11) and obtain [19]

$$\mathbf{z}_{uv} = \text{vec}(\mathbf{R}_{uv}) = \tilde{\mathbf{A}}_{uv} \mathbf{b}_{uv}, \quad (14)$$

where  $\tilde{\mathbf{A}}_{uv} = [\tilde{\mathbf{a}}_{uv}(\theta_1, \phi_1), \tilde{\mathbf{a}}_{uv}(\theta_2, \phi_2), \dots, \tilde{\mathbf{a}}_{uv}(\theta_L, \phi_L)]$  with  $\tilde{\mathbf{a}}_{uv}(\theta_l, \phi_l) = [\mathbf{a}^{(u)}(\theta_l, \phi_l)]^* \otimes \mathbf{a}^{(v)}(\theta_l, \phi_l)$ , and  $\mathbf{b}_{uv} = [\rho_1^{(uv)},$

$\dots, \rho_L^{(uv)}]^T$ . To employ the group LASSO for 2-D DOA estimation,  $K^2$  optimization vectors  $\mathbf{b}_{uv}^o$  with  $u, v \in [1, K]$ , each of size  $G \times 1$ , are initialized, where  $G$  is the total number of search grids for the DOAs. Let  $\mathbf{B}_{uv}$  denote the dictionary matrix corresponding to difference coarray between the  $u$ th and  $v$ th subarrays. The group sparsity problem can now be formulated as [11, 20]

$$\begin{aligned} \hat{\mathbf{b}}^o &= \\ &\arg \min_{\mathbf{b}^o} \sum_{u=1}^K \sum_{v=1}^K \|\mathbf{z}_{uv} - \mathbf{B}_{uv} \mathbf{b}_{uv}^o\|_2 + \xi \|\mathbf{b}_{uv}^o\|_{1,2}, \end{aligned} \quad (15)$$

where  $\mathbf{b}^o = [(\mathbf{b}_{11}^o)^T, \dots, (\mathbf{b}_{KK}^o)^T]^T$ ,  $\xi$  is a regularization parameter, and the mixed  $l_{1,2}$  norm of vector  $\mathbf{b}_{uv}^o$  is defined as

$$\|\mathbf{b}_{uv}^o\|_{1,2} = \sum_{a=1}^G \left( \sum_{i=1}^{K^2} \mathbf{B}(a, i) \mathbf{B}^*(a, i) \right)^{\frac{1}{2}}, \quad (16)$$

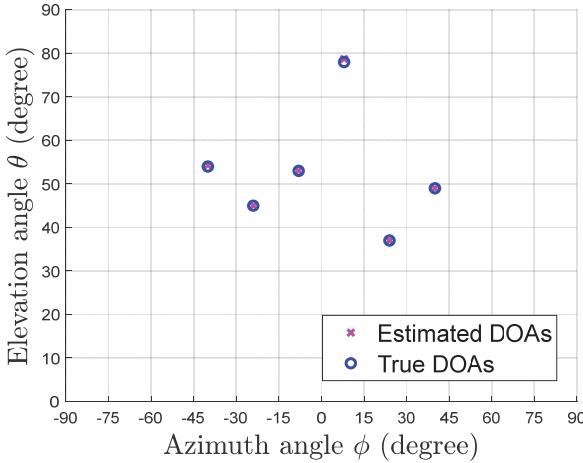
with  $\mathbf{B}$  denoting the matrix constructed by concatenating all the vectors  $\mathbf{b}_{uv}^o$ . The DOA estimates are given as the summed coefficients on the  $G$ -point grid, i.e.,

$$\hat{\mathbf{b}} = \sum_{u=1}^K \sum_{v=1}^K |\hat{\mathbf{b}}_{uv}^o|. \quad (17)$$

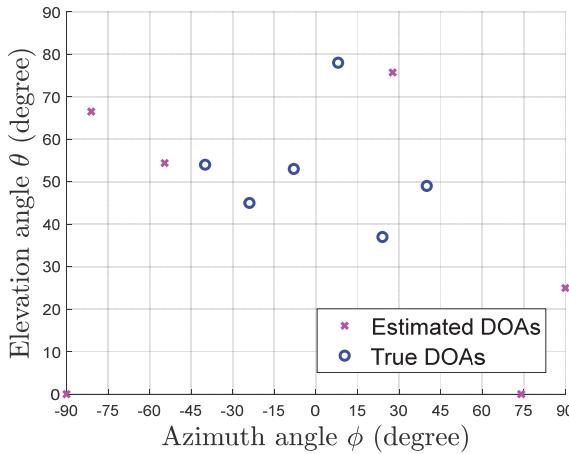
### V. SIMULATION RESULTS

We assume the array geometry as depicted in Fig. 1. There are  $K = 2$  sparse subarrays with  $M_1 = M_2 = 3$ . Take the orientation of the first node as the reference with  $\beta_1 = 0^\circ$ , and the orientation of the second subarray is chosen as  $\beta_2 = 45^\circ$ . Denoting a half-wavelength to be unity, the sensor locations of the first subarray are given as  $(x_{11}, y_{11}) = (0, 0)$ ,  $(x_{12}, y_{12}) = (1, 0)$ , and  $(x_{13}, y_{13}) = (3, 0)$ , and those of the second subarray are given as  $(x_{21}, y_{21}) = (6, 2)$ ,  $(x_{22}, y_{22}) = (6.707, 2.707)$ , and  $(x_{23}, y_{23}) = (8.121, 4.121)$ .  $L = 6$  uncorrelated signals are considered, and their elevation and azimuth angles are randomly chosen from  $\theta_l \in [0^\circ, 90^\circ]$  and  $\phi_l \in [-90^\circ, 90^\circ]$ , respectively, and are given as  $(\theta_1, \phi_1) = (54^\circ, -40^\circ)$ ,  $(\theta_2, \phi_2) = (45^\circ, -24^\circ)$ ,  $(\theta_3, \phi_3) = (53^\circ, -8^\circ)$ ,  $(\theta_4, \phi_4) = (78^\circ, 8^\circ)$ ,  $(\theta_5, \phi_5) = (37^\circ, 24^\circ)$ , and  $(\theta_6, \phi_6) = (49^\circ, 40^\circ)$ . It is noted that, in this case, the number of signals is higher than the number of degrees of freedom of the physical array, and DOA estimation is carried out by exploiting the difference coarray. We use 1,000 data samples, and the input signal-to-noise ratio (SNR) is 0 dB. The regularization parameter for the group LASSO is chosen to be  $\xi = 20$ .

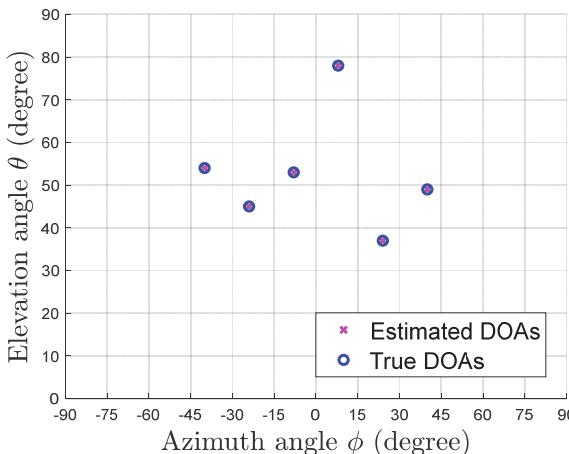
We first show the 2-D DOA estimation performance when the MUSIC algorithm is used and the phase difference between the two subarrays is precisely known. In this case, as shown in Fig. 2, all the DOAs of the 6 signals are detected successfully. In practice, however, the phase difference between the two subarrays is random and unavailable. When an inaccurate phase difference is assumed, MUSIC fails to locate the signal DOAs, as depicted in Fig. 3.



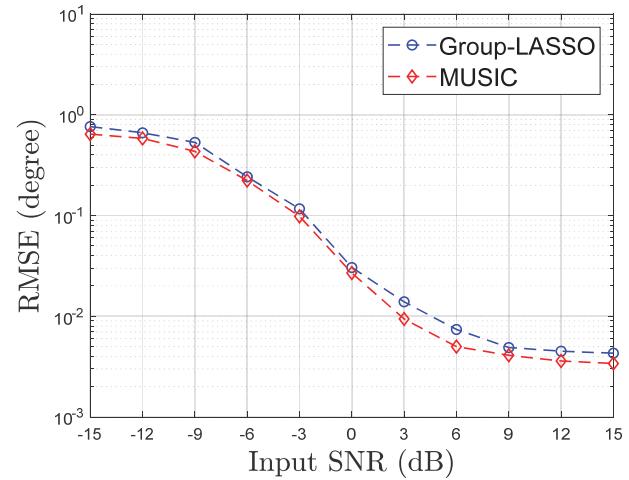
**Figure 2.** 2-D DOA estimation using MUSIC assuming precise knowledge of the phase difference between subarrays.



**Figure 3.** 2-D DOA estimation using MUSIC when an inaccurate phase difference between subarrays is assumed.



**Figure 4.** 2-D DOA estimation using group LASSO without knowledge of the phase difference between subarrays.



**Figure 5.** Comparison of RMSE performance of DOA estimation versus the input SNR for group LASSO and MUSIC with knowledge of the phase difference between subarrays.

Fig. 4 shows the 2-D DOA estimation results using the group LASSO when the phase difference between the two subarrays is unavailable. It is observed that all the sources are successfully detected, clearly depicting the robustness of the group sparsity-based approach to the unknown phase differences between distributed subarrays.

To analyze the DOA estimation performance of the group LASSO-based approach, we compare the root mean-square error (RMSE) results of both the group LASSO and MUSIC methods. The RMSE of estimated DOAs is defined as

$$\text{RMSE} = \sqrt{\frac{1}{NL} \sum_{n=1}^N \sum_{l=1}^L [(\hat{\theta}_{l,n} - \theta_l)^2 + (\hat{\phi}_{l,n} - \phi_l)^2]}, \quad (18)$$

where  $N$  is the number of Monte Carlo trials and  $(\hat{\theta}_{l,n}, \hat{\phi}_{l,n})$  represents the estimated elevation and azimuth DOAs of the  $l$ th trial.

In Fig. 5, the RMSE results obtained from both group LASSO and MUSIC are shown with respect to the input SNR, where the MUSIC algorithm assumes precise knowledge of the phase difference between the two subarrays. Each RMSE result is computed from 100 Monte Carlo trials. The input SNR varies between  $-15$  and  $15$  dB with an interval of  $3$  dB and the number of data samples assumed is  $1,000$ . It is note that, when the information of the phase difference between the subarrays is not available, the MUSIC algorithm does not resolve the signals and, as a result, its RMSE values are not included for comparison.

It can be observed that the performance of the group LASSO is very close to that of the 2-D MUSIC algorithm, verifying that group LASSO achieves near-coherent processing capability without requiring the knowledge of the phase difference between the two subarrays. As such, it removes the barriers of requiring

the precise phase difference between the subarrays as in the MUSIC algorithm, thereby enabling practical implementation for effective 2-D DOA estimation using distributed arrays.

## VI. CONCLUSION

We considered a 2-D DOA estimation problem using a distributed array, in which the subarrays have arbitrary orientations. Such a configuration of the distributed array differs from the well-studied collinearly or parallelly placed distributed arrays. The analysis of the array covariance matrix was provided with a focus on the impact of random phase differences in the cross-covariance matrix between a pair of subarrays. The group LASSO is used to perform group sparsity-based DOA estimation which achieves near-coherent processing capability without requiring the knowledge of the phase differences between subarrays. Simulation results verified the effectiveness of the proposed approach to achieve accurate 2-D DOA estimation.

## REFERENCES

- [1] M. Pesavento, A. B. Gershman, and K. M. Wong, "Direction finding in partly calibrated sensor arrays composed of multiple subarrays," *IEEE Trans. Signal Process.*, vol. 50, no. 9, pp. 2103–2115, Sept. 2002.
- [2] C. M. S. See and A. B. Gershman, "Direction-of-arrival estimation in partly calibrated subarray-based sensor arrays," *IEEE Trans. Signal Process.*, vol. 52, no. 2, pp. 329–338, Feb. 2004.
- [3] R. J. Kozick and B. M. Sadler, "Source localization with distributed sensor arrays and partial spatial coherence," *IEEE Trans. Signal Process.*, vol. 52, no. 3, pp. 601–616, March 2004.
- [4] F. Wen, Q. Wan, R. Fan, and H. Wei, "Improved MUSIC algorithm for multiple noncoherent subarrays," *IEEE Signal Process. Lett.*, vol. 21, no. 5, pp. 527–530, May 2014.
- [5] W. Suleiman, P. Parvazi, M. Pesavento, and A. M. Zoubir, "Non-coherent direction-of-arrival estimation using partly calibrated arrays," *IEEE Trans. Signal Process.*, vol. 66, no. 21, pp. 5776–5788, Nov. 2018.
- [6] M. W. T. S. Chowdhury and Y. D. Zhang, "Direction-of-arrival estimation exploiting distributed sparse arrays," in *Proc. Asilomar Conf. Signals, Systems, Comput.*, Pacific Grove, CA, Nov. 2021, pp. 231–235.
- [7] Y. D. Zhang and A. Prater-Bennette, "Collaborative direction-of-arrival estimation exploiting one-bit cross-correlations," in *Proc. Asilomar Conf. Signals, Systems, Comput.*, Pacific Grove, CA, Nov. 2021, pp. 236–240.
- [8] M. W. T. S. Chowdhury and Y. D. Zhang, "Cramer-Rao bound analysis of distributed DOA estimation exploiting mixed-precision covariance matrix," in *Proc. IEEE Int. Conf. Acoust., Speech Signal Process.*, Singapore, 2022, pp. 5163–5167.
- [9] A. J. Small, "Radio frequency emitter geolocation using CubeSats," master's thesis, Air Force Institute of Technology, 2014.
- [10] Z. Wang, E. Blasch, G. Chen, D. Shen, X. Lin, and K. Pham, "A low-cost, near-real-time two-UAS-based UWB emitter monitoring system," *IEEE Aerosp. Electron. Syst. Mag.*, vol. 30, no. 11, pp. 4–11, 2015.
- [11] A. Hassani, J. Plata-Chaves, M. H. Bahari, M. Moonen, and A. Bertrand, "Multi-task wireless sensor network for joint distributed node-specific signal enhancement, LCMV beamforming and DOA estimation," *IEEE J. Sel. Topics Signal Process.*, vol. 11, no. 3, pp. 518–533, April 2017.
- [12] A. Ahmed, S. Zhang, and Y. D. Zhang, "Multi-target motion parameter estimation exploiting collaborative UAV network," in *Proc. IEEE Int. Conf. Acoust., Speech Signal Process.*, Brighton, U.K., May 2019, pp. 4459–4463.
- [13] D. Fan, G. Guo, J. Song, L. Li, and Y. Zhu, "DOA estimation for arbitrarily distributed subarrays in UAV swarm," in *Proc. IEEE/CIC Int. Conf. Commun. China*, Chongqing, China, Aug. 2022, pp. 794–799.
- [14] S. Qin, Y. D. Zhang, and M. G. Amin, "Improved two-dimensional DOA estimation using parallel coprime arrays," *Signal Processing*, vol. 172, pp. 1–9, July 2020.
- [15] G. Zhang, T. Huang, Y. Liu, X. Wang, and Y. C. Eldar, "Direction finding in partly calibrated arrays exploiting the whole array aperture," *IEEE Trans. Aerosp. Electron. Syst.*, vol. 59, no. 5, pp. 5978–5992, Oct. 2023.
- [16] D. Garren, U. Majumder, and E. Blasch, *Essential Principles of Signals Collection and Analysis*, Artech House, 2023.
- [17] Q. Shen, W. Liu, W. Cui, S. Wu, Y. D. Zhang, and M. G. Amin, "Low-complexity wideband direction-of-arrival estimation based on co-prime arrays," *IEEE/ACM Trans. Audio, Speech and Language Process.*, vol. 23, no. 9, pp. 1445–1456, Sept. 2015.
- [18] S. Qin, Y. D. Zhang, M. G. Amin, and B. Himed, "DOA estimation exploiting a uniform linear array with multiple coprime frequencies," *Signal Process.*, vol. 130, pp. 37–46, Jan. 2017.
- [19] A. Ahmed, D. Silage, and Y. D. Zhang, "High-resolution target sensing using multi-frequency sparse array," in *Proc. IEEE Sensor Array Multich. Signal Process. Workshop*, Hangzhou, China, 2020, pp. 1–5.
- [20] S. Zhang, A. Ahmed, Y. D. Zhang, and S. Sun, "Enhanced DOA estimation exploiting multi-frequency sparse array," *IEEE Trans. Signal Process.*, vol. 69, pp. 5935–5946, Oct. 2021.
- [21] Q. Wu, Y. D. Zhang, M. G. Amin, and B. Himed, "High-resolution passive SAR imaging exploiting structured Bayesian compressive sensing," *IEEE J. Sel. Topics Signal Process.*, vol. 9, no. 8, pp. 1484–1497, Dec. 2015.
- [22] L. Meier, S. V. D. Geer, and P. Bühlmann, "The group lasso for logistic regression," *J. R. Statist. Soc. B*, vol. 70, no. 1, Feb. 2008, pp. 53–71.
- [23] N. Simon and R. Tibshirani, "Standardization and the group lasso penalty," *Stat. Sin.*, vol. 22, no. 3, pp. 983–1001, June 2012.
- [24] P. Pal and P. P. Vaidyanathan, "Nested arrays: A novel approach to array processing with enhanced degrees of freedom," *IEEE Trans. Signal Process.*, vol. 58, no. 8, pp. 4167–4181, Aug. 2010.
- [25] P. P. Vaidyanathan and P. Pal, "Sparse sensing with co-prime samplers and arrays," *IEEE Trans. Signal Process.*, vol. 59, no. 2, pp. 573–586, Feb. 2011.
- [26] S. Qin, Y. D. Zhang, and M. G. Amin, "Generalized coprime array configurations for direction-of-arrival estimation," *IEEE Trans. Signal Process.*, vol. 63, no. 6, pp. 1377–1390, March 2015.
- [27] A. Ahmed and Y. D. Zhang, "Generalized non-redundant sparse array designs," *IEEE Trans. Signal Process.*, vol. 69, pp. 4580–4594, Aug. 2021.